26. Fundamental Theory of Toothed Gearing (IV).

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We have developed the general theory of profile curves in the preceding reports from (I) to (III).¹⁾ Now we shall give its several applications to practical curves.

§ 1. Profile curves of cycloidal system.

Take a circle with radius a_{γ} as a rolling curve K_{γ} . However, in this case, as a pitch curve K we may not necessarily take a circle. Suppose that K_{γ} (and accordingly K) is oriented as a_{γ} is positive, that is, the direction of K_{γ} is positive, if the center Oof the circle K_{γ} always exists on the left side to the direction. From the two points at which the straight line connecting the center O_{γ} of K_{γ} with a drawing point C invariably connected with K_{γ} intersects the perimeter of K_{γ} we choose the nearer one to C, denoting it by P_0 and adopt P_0 as origin. And denote by s the length of arc measured from the origin to an arbitrary point P on K_{γ} . Denote by r the signed length of the segment PC and by θ the angle between the straight line PC and the tangent to K_{γ} at P, where $sgn(\theta)$ =sgn(r).

If we find the relation r=f(s) between r and s and the relation $r=g(\theta)$ between r and θ , they are respectively the equations of the profile curve F drawn by the drawing point C and of the path of contact Γ corresponding to F.

Now from the triangle $O_{\gamma}PC$ we have

 $PC^2 = O_{\gamma}C^2 + O_{\gamma}P^2 - 2O_{\gamma}C \cdot O_{\gamma}P \cos C\hat{O}_{\gamma}P$

and then denoting by e the length of the spgment P_0C

 $r^2 = e^2 + 4a_{\gamma}(a_{\gamma} - e)\sin^2 \frac{s}{2a_{\gamma}}$

Hence, when e > 0

(1)₁
$$r = f(s) = \sqrt{e^2 + 4a_\gamma(a_\gamma - e)\sin^2\frac{s}{2a_\gamma}}$$

and when e < 0

(1)₂
$$r = f(s) = \begin{cases} -\sqrt{e^2 + 4a_\gamma(a_\gamma - e)\sin^2 \frac{s}{2a_\gamma}}, \text{ where } |s| \leq a_\gamma \cos^{-1} \left(\frac{a_\gamma}{a_\gamma - e}\right) \\ \sqrt{e^2 + 4a_\gamma(a_\gamma - e)\sin^2 \frac{s}{2a_\gamma}}, \text{ where } |s| \geq a_\gamma \cos^{-1} \left(\frac{a_\gamma}{a_\gamma - e}\right) \end{cases}$$

In particular, when e=0, that is, the drawing point C exists on the perimeter of K_{γ} ,

¹⁾ This Proceedings, Vol. 25 (1949). No. 2.

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(1)₃
$$r = f(s) = 2a_{\gamma} \sin \frac{|s|}{2a_{\gamma}}$$

Next, from the same triangle $O_{\gamma}PC$ we have

$$PC^{2} = O_{\gamma}C^{2} - O_{\gamma}P^{2} + 2PC \cdot O_{\gamma}P \cos O_{\gamma}\hat{P}C,$$

that is,

(2) $r^2 - 2a_{\gamma}\sin\theta \cdot r + e(2a_{\gamma} - e) = 0,$

The curve denoted by (2), namely, the path of constact Γ is a circular arc with the point O_{γ} as its center and $a_{\gamma}-e$ as its radius. This is the fact that we can again immediately derive from the characteristic property of path of contact which we have explained in the report (II) § 4, for the evolute of the circle K_{γ} is reduced to its center O_{γ} . From (2) we have

when e > 0

(2)₁
$$r=g(\theta)=a_{\gamma}\sin\theta\pm\sqrt{a_{\gamma}^{2}\sin^{2}\theta-e(2a_{\gamma}-e)},$$

and when e > 0

(2)₂
$$r = g(\theta) = \begin{cases} a_{\gamma} \sin \theta + \sqrt{a_{\gamma}^2 \sin^2 \theta - e(2a_{\gamma} - e)} , \text{ where } \theta \ge 0, \\ -a_{\gamma} \sin \theta - \sqrt{a_{\gamma}^2 \sin^2 \theta - e(2a_{\gamma} - e)}, \text{ where } \theta \le 0. \end{cases}$$

In particular, when e=0, that is, the drawing point C exists on the perimeter of K_{γ} ,

(2)₃
$$r = g(\theta) = 2a_{\gamma} \sin \theta$$
, where $\theta \ge 0$

 $(2)_{s}$ is the equation of the rolling curve K_{r} itself.

Next, let the natural equations of the pitch curves K_1 and K_2 be $a_1=a_1(s)$, $a_2=a_2(s)$ respectively, then by Equation (13) in the report (III) we have the specific slidings σ_1 and σ_2 of the profile curves F and F as follows :

(3)
$$\sigma_1 = \sigma_1(s) = \frac{\frac{1}{a_1(s)} - \frac{1}{a_2(s)}}{\frac{1}{a_{\gamma}} - \frac{1}{a_2(s)}}, \ \sigma_2 = \sigma_2(s) = \frac{\frac{1}{a_2(s)} - \frac{1}{a_1(s)}}{\frac{1}{a_{\gamma}} - \frac{1}{a_2(s)}},$$

The values of σ_1 and σ_2 are independent of the position of the given drawing point C.

From (3) it follows :

When the rolling curve K_r is a circle and moreover both of the pitch curves K_1 and K_2 are circles, then both of the specific slidings σ_1 and σ_2 become constant. Conversely, suppose that both of the pitch curves K_1 and K_2 are circles. If the profile curves F_1 and F_2 have constant specific slidings σ_1 and σ_2 , then the rolling curve K_r corresponding to F_1 and F_2 is necessarily a circle.²⁾

§ 2. Circular and straight profile curves.

Take a circle with radius a as a pitch curve K and settle a

²⁾ T. Kubota : Geometry of Gears (Japanese), (1947), p. 112.

circular arc F with a point M as its center and m as its radius at K as a profile curve. When the point M exists at the inside of the circle K, we can adopt an arbitrary arc of the circle F as a profile curve. When M exists at the outside of K, we can adopt a part of the arc between the two tangents drawn M to K as a profile curve. When M exists on the perimeter of K, we can not adopt any arc of F as a profile curve (making one-point contact).

Let the circle K be oriented as the radius a is positive, and take the nearer point P_0 to M as origin from the two points at which the straight line connecting the center O of K with the center M of F intersects the perimeter of K. Denote by e the length of the segment P_0M .

Now we may conclude that the arc F is the parallel profile curve with the distance m to the point M. In this case, the direction of F is necessarily determined and accordingly the sign of m. Hence, from Equation (1), we have immediately the equation of F by Equation (3) in the report (II) as follows : When e > 0

(4)₁
$$r = f(s) = \pm m + \sqrt{e^2 + 4a(a-e)\sin^2\frac{s}{2a}}$$
,

and when e > 0

(4)₂
$$r=f(s) = \begin{cases} -m - \sqrt{e^2 + 4a(a-e)\sin\frac{s}{2a}}, \text{ where } |s| \leq a\cos^{-1}\left(\frac{a}{a-e}\right), \\ -m + \sqrt{e^2 + 4a(a-e)\sin\frac{s}{2a}}, \text{ where } |s| \geq a\cos^{-1}\left(\frac{a}{a-e}\right). \end{cases}$$

The path of contact Γ of F is the conchoid curve, having the distance m, of the circular arc with the point O as the center and a-e as the radius. And the equation of Γ is derived from (2) by Equation (11) in the report (II) : When e > 0

(5), $r = g(\theta) = \pm m + a \sin \theta \pm \sqrt{a^2 \sin^2 \theta} - e(2a - e)$, and when e > 0

(5)₂
$$r = g(\theta) = \begin{cases} -m + a \sin\theta + \sqrt{a^2 \sin^2\theta} - e(2a - e), & \text{where } \theta \ge 0, \\ -m - a \sin\theta - \sqrt{a^2 \sin^2\theta} - e(2a - e), & \text{where } \theta \le 0. \end{cases}$$

Now, if |e| is sufficiently large, then trasforming the first equation of $(4)_2$, we have

$$r = f(s) = -m + e\sqrt{1 + 4 \frac{a(a-e)}{e^2} \sin^2 \frac{s}{2a}}$$

= $-m + e - a(1 - \cos \frac{s}{a}) + \frac{1}{e} \left[2a^2 \sin^2 \frac{s}{2a} - 2 \frac{a^2(a-e)^2}{e^3} \sin^4 \frac{s}{2a} + \cdots \right],$

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that is,

(6)
$$r=f(s)=-b+a\cos\frac{s}{a}+\frac{1}{e}\left[2a^{2}\sin^{2}\frac{s}{2a}+\cdots\right],$$

where b=m-e+a denotes the distance from the point O to the circle F. In (6), if $m \to -\infty$ and accordingly $e \to -\infty$ then the arc F becomes a part of the straight line with the distance b from O and its equation is given by

(7)
$$r=f(s)=a\cos\frac{s}{a}-b.$$

The path of contact Γ of this straight profile curve F is derived by making $m \rightarrow -\infty$ in (5), or from (7) using the relation $\frac{s}{a} = sgn(\theta) - \frac{\pi}{2} - \theta:$ (8) $r = g(\theta) = a |\sin \theta| - b.$

If we take one of the points of intersection of F and K as origin, from (7) we have the following equation (9) by substituting s+a $a\cos^{-1}\frac{b}{a}$ or $s-a\cos^{-1}\frac{b}{a}$ into (7) in place of s:

(9)
$$r = f(s) = a \cos\left(\frac{s}{a} \pm \cos^{-1}\frac{b}{a}\right) - b$$

or

(10)
$$r=f(s)=a\sin\frac{s}{a}\sin\theta_0-b\left(1-\cos\frac{s}{a}\right),$$

where θ_0 denotes the angle between F and K. If, at this time, $a \rightarrow \infty$, then we have

 $r = f(s) = s \sin \theta_0$.

(11)

§ 3 Involute profile curves.

There exist two involutes drawn out from an arbitrary point I on a circle. When we regard these two involutes together as a curve, the point I is a cusp of this curve. If needed, we shall call the two involutes the branch cuves of this composed curve. Equation (11) in § 2 is the equation of the straight line F which intersects a straight line K at the angle of intersection θ_0 , when we take K as a pitch curve and F as a profile curve. If we take a circle O_1 with radius a_1 as a pitch curve corresponding to K, then the profile curve corresponding to the straight line F is a (composed) involute F_1 of the circle which has the radius $|a_1 \sin \theta_0|$ and concentric with the pitch circle O_1 . In this case, we shall give the notice that, depending on the length of the straight profile curve F, we should take a part of one of the two branches of F_1 as the profile curve corresponding to F or a part of F_1 extending the two branches. If we take another circle O_2 with radius a_2 as a pitch curve, then the profile curve F_2 corresponding to F is a (composed) involute of the circle which has the radius $|a_2 \sin \theta_0|$ and concentric

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with O_2 . By the generalized Camus' theorem in the report (I), the two (composed) involutes F_1 and F_2 become a pair of profile curves, when we take the circles O_1 and O_2 as a pair of pitch curves. And the path of contact Γ is, in this case, the straight line perpendicular to the straight line F:

(12)
$$r = g(\theta) : \theta = \theta_0 + sgn(\theta_0)sgn(s)\frac{\pi}{2} .$$

Next, the equation of the rolling curve K_{γ} is given by the above equation (11) and Equation (8) in the report (II) or by the above equation (12) and Equation (5) in the report (II) as follows :

(13)
$$a_r = a_r(s) = \frac{r}{\cos \theta_0} = s \tan \theta_0$$

In accordance with Equation (4) in the report (III), the velocity of sliding of the point of contact C of F_1 and F_2 is given by

(14)
$$v_p = \pm \left(\frac{1}{a_1} - \frac{1}{a_2}\right) \sin \theta_0 \frac{ds}{dt} s.$$

In particular, when the pitch circles O_1 and O_2 rotate with constant angular velocities, the accelerations of sliding of the profile curves have the components by Equation (6) in the report (II) :

(15)
$$w_t = \pm \left(\frac{1}{a_1} - \frac{1}{a_2}\right) \left(\frac{ds}{dt}\right)^2 \sin \theta_0$$

and

(16)₁
$$w_{n1} = \left(\frac{1}{a_1} - \frac{1}{a_2}\right)^2 \left(\frac{ds}{dt}\right)^2 \frac{r^2}{a_2 \cos \theta_0 - r}$$

or

(16)₂
$$w_{n2} = \left(\frac{1}{a_2} - \frac{1}{a_1}\right)^2 \left(\frac{ds}{dt}\right)^2 \frac{r^2}{a_1 \cos \theta_0 - r}.$$

From (15) it follows that the profile curves slide one along the other with constant tangential acceleration.

Furthermore, by Equation (14) in the report (III), the specific slidings of F_1 and F_2 are respectively given by

(17)
$$\sigma_{1} = \frac{\frac{1}{a_{1}} - \frac{1}{a_{2}}}{\frac{\cos \theta_{0}}{r} - \frac{1}{a_{1}}}, \quad \sigma_{2} = \frac{\frac{1}{a_{2}} - \frac{1}{a_{1}}}{\frac{\cos \theta_{0}}{r} - \frac{1}{a_{2}}}.$$

Now denote by C_2 the point which is on F_2 and corresponds to the cusp I_1 of F_1 , the starting point on the base circle of the two branch curves of F_1 and by C_1 the point which is on F_1 and corresponds to the cusp I_2 of F_2 . When the point of contact C of F_1 and F_2 runs on F_1 from the point I_1 to the point C_1 , the point

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C runs on the branch curve of F_2 on which the point C_2 exists from C_2 to the point I_2 . Furthermore, if C continues to run on F_1 , then on F_2 C runs on another branch curve of F_2 starting from I_2 .

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