

Research Article

A Method to Determine Oscillation Emergence Bifurcation in Time-Delayed LTI System with Single Lag

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One type of bifurcation named oscillation emergence bifurcation (OEB) found in time-delayed linear time invariant (abbr. LTI) systems is fully studied. The definition of OEB is initially put forward according to the eigenvalue variation. It is revealed that a real eigenvalue splits into a pair of conjugated complex eigenvalues when an OEB occurs, which means the number of the system eigenvalues will increase by one and a new oscillation mode will emerge. Next, a method to determine OEB bifurcation in the time-delayed LTI system with single lag is developed based on Lambert W function. A one-dimensional (1-dim) time-delayed system is firstly employed to explain the mechanism of OEB bifurcation. Then, methods to determine the OEB bifurcation in 1-dim, 2-dim, and high-dimension time-delayed LTI systems are derived. Finally, simulation results validate the correctness and effectiveness of the presented method. Since OEB bifurcation occurs with a new oscillation mode emerging, work of this paper is useful to explore the complex phenomena and the stability of time-delayed dynamic systems.

1. Introduction

In the nature, system trend is not only dependent on the current operating point but also subject to its previous conditions. This phenomenon is called time delay [1, 2]. As a main cause to the control deterioration and system instability, time delays exist widespread in the industry of communication [3], biology [4], mechanism [5], chemistry [6], society [7], and power utility [8–10]. Therefore, it is an important issue and frequent topic to evaluate the impact of time delays on the stability of dynamic systems.

Many methods to analyze the stability of time-delayed dynamic system have been proposed in the past literatures. For example, [10–13] applied Lyapunov theory to derive various stability criteria for time-delayed systems. To seek the suitable Lyapunov function (or Lyapunov functional) and to construct the corresponding criteria were the two key points of such methods. Linear matrix inequality (LMI) technique, Lyapunov-Razumikhin theory, and Lyapunov-Krasovskii theory were usually used in the derivation. Just as we know, characteristic equation of time-delayed system has transcendental element, which is very difficult to handle in the analysis. In order to surmount this problem, [14, 15]

utilized Rekasius substitution method and [16] used Pade approximation method to approximate the transcendental elements and transfer the characteristic equation into a polynomial, which was used to calculate the system critical eigenvalues. Reference [9, 17] treated the stability region method as a tool to determine the small signal stability region of time-delayed dynamic system. All points in the stability region were small signal stable, and the boundary of the stability region was composed by some bifurcation points, such as saddle node bifurcation, Hopf bifurcation, and singularity induced bifurcation. Reference [18–22] applied bifurcation theory to analyze some complex phenomena existing in the time-delayed systems, such as Hopf bifurcation, period doubling bifurcation, and chaos.

Time-delayed system is a complex dynamic system, in which many interesting and intricate dynamic behaviors exist. For example, Figure 1 from [23] demonstrated that a real eigenvalue split into a pair of conjugated complex eigenvalues at point P with increase of time delay in a time-delayed power system. In this paper, this phenomenon is called oscillation emergence bifurcation (OEB). And, we apply the theory of bifurcation analysis and Lambert W function to propose a mechanism to the occurrence of this bifurcation. As

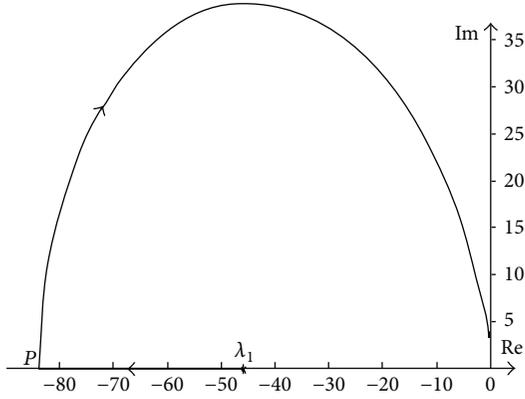


FIGURE 1: A real eigenvalue splits into a pair of conjugated eigenvalues.

an available tool, Lambert W function [24, 25] has been utilized to analyze some complex behaviors in nonlinear system including stability analysis of time-delayed system [26–29]. It is applied to derive a general method to determine OEB bifurcation in this paper.

The contents of this paper are organized into six sections. Following this introduction, definition of OEB bifurcation is put forward in Section 2 and some of its features are also discussed in this section. In Section 3, Lambert W function is introduced and a mechanism of the OEB's occurrence is proposed. Section 4 presents a method to determine OEB bifurcation in time-delayed LTI system with single lag based on the Lambert W function. In Section 5, the presented approach is demonstrated by numerical simulations. Finally, Section 6 concludes and summarizes this paper.

2. Definition of OEB Bifurcation

In this paper, all studies are based on the following time-delayed LTI system with single lag:

$$\Sigma: \begin{cases} \dot{\mathbf{x}} = \mathbf{A}_0 \cdot \mathbf{x} + \mathbf{A}_i \cdot \mathbf{x}(t - \tau) \\ \mathbf{x}(t) = \boldsymbol{\phi}(t), \quad t \in [-\tau, 0], \end{cases} \quad (1)$$

where $\mathbf{A}_0, \mathbf{A}_i \in R^{n \times n}$; $\mathbf{x} \in R^n$ is the vector of the state variables; $\tau \geq 0$ is the constant of time delay; $\boldsymbol{\phi}(t)$ is the system trajectory in the range of $[-\tau, 0]$.

It is well known that the following equation is the corresponding characteristic equation of system Σ :

$$\det(s - \mathbf{A}_0 - \mathbf{A}_i \cdot e^{-s\tau}) = 0, \quad (2)$$

where $s \in C$ is the eigenvalue to be determined. The eigenvalue spectrum of system Σ is denoted by Γ :

$$\Gamma = [s_1, s_2, s_3, \dots]. \quad (3)$$

Theoretically, it can be calculated from (2) directly when τ is given. Further, denote the set of the real eigenvalue by Γ_R and

the set of the complex eigenvalue with nonzero imaginary by Γ_I :

$$\begin{aligned} \Gamma_R &= [s_1, s_2, \dots, s_{n_R}], \\ \Gamma_I &= [\tilde{s}_1, \tilde{s}_2, \dots, \tilde{s}_{n_I}], \end{aligned} \quad (4)$$

where n_R, n_I are the eigenvalue numbers of Γ_R and Γ_I , respectively. Then the following (5) holds:

$$\begin{aligned} \Gamma &= [\Gamma_R, \Gamma_I], \\ n_\tau &= n_R + n_I, \end{aligned} \quad (5)$$

where n_τ is the eigenvalue number of Γ .

It can be found that when $\tau = 0$, system Σ degenerates into the following LTI differential equation:

$$\dot{\mathbf{x}} = \mathbf{A} \cdot \mathbf{x}, \quad (6)$$

where $\mathbf{A} = \mathbf{A}_0 + \mathbf{A}_i$. And, the number of eigenvalues is n ; that is, $n_{\tau=0} = n$. When τ increases, the values of n_R, n_I , and n_τ will change accordingly. Therefore, they can be considered as functions of τ as follows:

$$\begin{aligned} n_R &= N_R(\tau), \\ n_I &= N_I(\tau), \\ n_\tau &= N(\tau) = N_R(\tau) + N_I(\tau). \end{aligned} \quad (7)$$

$N_R(\tau), N_I(\tau)$, and $N(\tau)$ are three functions of τ to yield the numbers of real eigenvalues, complex eigenvalues, and whole eigenvalues of system Σ .

Definition 1 (definition of oscillation emergence bifurcation). Presume that there is a value of time delay $\tau_c > 0$ for system Σ of (1). Its Γ_R has n_R^o real eigenvalues and Γ_I has n_I^o complex eigenvalues with $\tau \leq \tau_c$. And, after $\tau > \tau_c$, the numbers of Γ_R and Γ_I turn to n_R^n and n_I^n . If the following equations hold:

$$\begin{aligned} n_R^n &= n_R^o - 1, \\ n_I^n &= n_I^o + 2, \\ n_\tau^n &= n_\tau^o + 1, \\ n_\tau^n &= n_R^n + n_I^n, \\ n_\tau^o &= n_R^o + n_I^o, \end{aligned} \quad (8)$$

there is an oscillation emergence bifurcation at $\tau = \tau_c$.

According to Definition 1, suppose there is a real eigenvalue $s \in R$ in Γ at $\tau \leq \tau_c$. It will split into a pair of conjugated eigenvalues s_+, s_- as shown in Figure 2. It is manifested that the number of Γ_R will decrease by one, the number of Γ_I will increase by two, and number of Γ will increase by one after an OEB bifurcation occurs. At the same time, a new oscillation mode subject to s_+, s_- will emerge after OEB bifurcation.

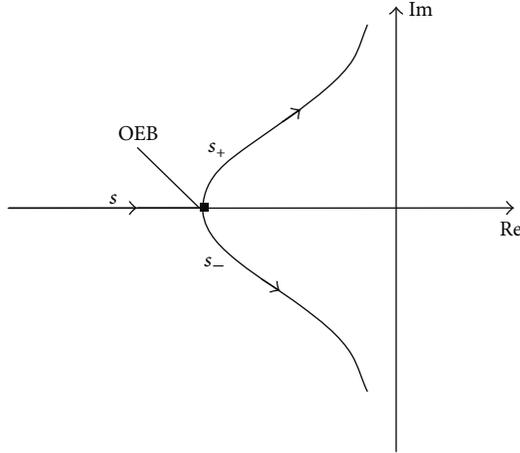


FIGURE 2: Illustration of OEB bifurcation.

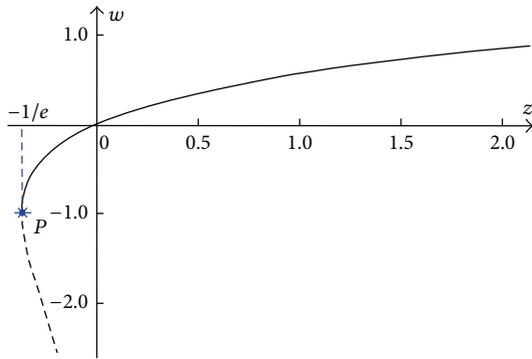


FIGURE 3: W_0 and W_{-1} branches of Lambert W function.

3. Lambert W Function and OEB Bifurcation

Our aim is to derive a general method based on Lambert W function to determine OEB bifurcation in system Σ defined by (1). A brief introduction to Lambert W function is firstly given.

The following function is called Lambert W function:

$$we^w = z, \tag{9}$$

where $w, z \in \mathbb{C}$. Its inverse function is expressed as

$$w = W(z), \quad \text{that is, } W(z)e^{W(z)} = z. \tag{10}$$

Lambert W function is not injective and the relation W is multivalued (except at 0). It has many solution branches in complex plane [25], which can be denoted by $W_k, k = 0, \pm 1, \pm 2, \dots$. If the attention is restricted to real-valued W , then the relation is defined only for $z \geq -1/e$. For $-1/e \leq z < 0$, there are two possible real values of $W(z)$ as shown in Figure 3. We denote the branch satisfying $-1 \leq W(z)$ by W_0 (solid line in Figure 3), and the branch satisfying $W(z) \leq -1$ by W_{-1} (dashed line in Figure 3). W_0 is referred to the principal branch of Lambert W function. It increases from $W_0(-1/e) = -1$ to $W_0(+\infty) = +\infty$, while branch W_{-1} decreases from $W_{-1}(-1/e) = -1$ to $W_{-1}(0_-) = -\infty$. They

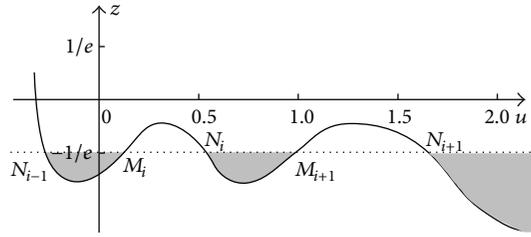


FIGURE 4: Curve of $z = f_z(u)$.

encounter at point P as shown in Figure 3, and the value of point P is given as follows:

$$P : (z, w) = \left(-\frac{1}{e}, -1\right). \tag{11}$$

Supposed that $z \in \mathbb{R}$ in (9) and (10) is a system parameter and it varies with another parameter $u \in \mathbb{R}$:

$$z = f_z(u), \quad z \in \mathbb{R}. \tag{12}$$

Substitute (12) into (10). It can be found that w is also a function of u :

$$w = W(z) = W(f_z(u)) = W_z(u). \tag{13}$$

Then, the u - z curve can be plotted. An example is shown in Figure 4, where u - z curve crosses the dotted line of $z = -1/e$ at some points which can be divided into two categories:

$$\begin{aligned} M_s &= (M_1, M_2, \dots, M_i, \dots), \\ N_s &= (N_1, N_2, \dots, N_i, \dots). \end{aligned} \tag{14}$$

If u is on the interval of (M_i, N_i) , that is, the intervals above the line with $z > -1/e$, (13) has real solutions. While if u is on the interval of (N_i, M_{i+1}) , that is, the grey intervals with $z < -1/e$, (13) only has complex solutions with nonzero imaginary.

Recalling the definition of OEB, we can find that N_s is just a set of OEB bifurcations of the system expressed by (13). That is, at any point of N_s , a real eigenvalue will turn into a pair of conjugated complex eigenvalues with the increment of u .

Here the following typical transcendental item in one-dimensional (1-dim) delayed-system is treated as an example for further discussion to Figure 4:

$$e^{-\tau s} = a_0(s - r), \tag{15}$$

where $a_0, r \in \mathbb{R}$, and $\tau \geq 0$. The value of s can be derived from (15) based on Lambert W function as follows:

$$s = r + \frac{1}{\tau} W\left(\frac{\tau e^{-\tau r}}{a_0}\right) = r + \frac{1}{\tau} W(z), \tag{16}$$

where

$$z = f_z(\tau) = \frac{\tau e^{-\tau r}}{a_0}. \tag{17}$$

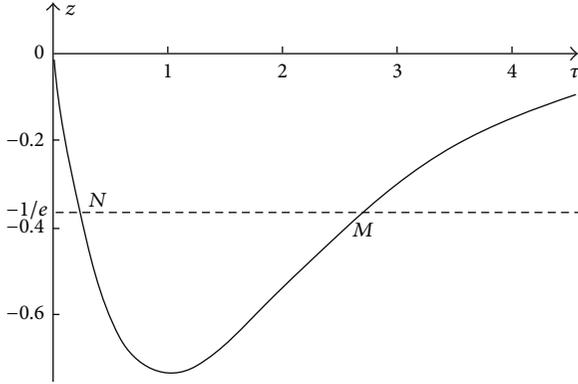
FIGURE 5: Curve of $z = f_z(\tau)$.

Figure 5 depicts the curve of τ - z with $a_0 = -0.5$, $r = 1.0$. It is evident that point N with $\tau = 0.23196$ in the figure is an OEB bifurcation of system (15) according to Definition 1 and Figure 4.

From Figures 4 and 5, it is asserted that the following formula holds at the OEB bifurcation points when $f_z(\cdot) \in \mathbb{R}$:

$$z = -\frac{1}{e}, \quad (18)$$

$$\frac{dz}{d\tau} = \frac{df_z}{d\tau} < 0.$$

And, if $f_z(\cdot)$ has complex values on one side of the OEB bifurcation point, the above condition will be modified as follows:

$$z = -\frac{1}{e}, \quad (19)$$

$$\frac{d \operatorname{Re}(z)}{d\tau} = \frac{d \operatorname{Re}(f_z)}{d\tau} < 0,$$

where $\operatorname{Re}(z)$ is the real part of z . For a time-delayed system, if its characteristic equation can be transformed into a suitable form, conditions of (18) or (19) may be adopted as a criterion to determine the OEB bifurcation.

4. An Approach to Determine OEB Bifurcation

In this section, we aim to derive a general method to transform the characteristic equation of time-delayed system into a form that can be handled by Lambert W function so as to determine the occurrence of OEB bifurcation. Methods suitable for one-dimensional (1-dim) and two-dimensional (2-dim) time-delayed LTI systems are first derived and then they are expanded to the high-dimensional systems.

4.1. 1-Dim System. The following 1-dim system is considered in this subsection:

$$\dot{x} = ax + bx(t - \tau), \quad (20)$$

where $\tau \geq 0$, $a, b, x \in \mathbb{R}$, and $b \neq 0$. The characteristic equation of (20) is

$$CE_1(s, D) = s - a - b \cdot D = 0, \quad (21)$$

where $D = e^{-\tau s}$. It can be rewritten as

$$D = e^{-\tau s} = \frac{1}{b}(s - a). \quad (22)$$

According to (15), s can be solved from (22) based on Lambert W function:

$$s = a + \frac{W(z)}{\tau}, \quad (23)$$

where

$$z = f_z(\tau) = b \cdot \tau \cdot e^{-\tau a}. \quad (24)$$

Similar to Figure 5, the OEB bifurcation can be determined from (24) via condition (18).

4.2. 2-Dim System. Let us consider the following 2-dim system:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix} \begin{bmatrix} x_1(t - \tau) \\ x_2(t - \tau) \end{bmatrix}, \quad (25)$$

where $\tau \geq 0$, $a_{ij}, b_{ij} \in \mathbb{R}$, $i, j = 1, 2$; $\mathbf{x} = [x_1, x_2]^T \in \mathbb{R}^2$. Assume $s_1 < s_2 < 0$ are two eigenvalues of the following matrix:

$$\tilde{\mathbf{A}} = \begin{bmatrix} a_{11} + b_{11} & a_{12} + b_{12} \\ a_{21} + b_{21} & a_{22} + b_{22} \end{bmatrix}. \quad (26)$$

It means that there are two negative and real eigenvalues at $\tau = 0$, so system given by (25) is stable without time delay. Supposed that s is an eigenvalue of (25) at $\tau > 0$ and the following equation holds:

$$\det \left\{ \begin{bmatrix} s - a_{11} & -a_{12} \\ -a_{21} & s - a_{22} \end{bmatrix} - \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix} e^{-\tau s} \right\} = 0. \quad (27)$$

System characteristic equation can be derived as follows:

$$CE_2(s, D) = s^2 + c_1 s + c_2 + c_3 D s + c_4 D + c_5 D^2 = 0. \quad (28)$$

With $c_1 = -(a_{11} + a_{22})$, $c_2 = a_{11}a_{22} - a_{12}a_{21}$, $c_3 = -(b_{11} + b_{22})$, $c_4 = a_{11}b_{22} + a_{22}b_{11} - (a_{12}b_{21} + a_{21}b_{12})$, $c_5 = b_{11}b_{22} - b_{12}b_{21}$, and $D = e^{-\tau s}$.

In order to determine the OEB bifurcation in the system, we reorganize (28) into the following form:

$$(s + \zeta + w \cdot D)(s + z + y \cdot D) - v = 0, \quad (29)$$

where $\zeta, y, w, v, z \in \mathbb{R}$. And, it can be expanded as follows:

$$s^2 + (\zeta + z)s + (\zeta z - v) + (w + y)Ds + (wz + \zeta y)D + wyD^2 = 0. \quad (30)$$

Comparing (30) with (28), the following equations hold:

$$\begin{aligned} \zeta + z &= c_1, \\ \zeta z - v &= c_2, \\ w + y &= c_3, \\ wz + \zeta y &= c_4, \\ wy &= c_5. \end{aligned} \tag{31}$$

And, the following result can be obtained:

$$\begin{aligned} w &= \frac{c_3 \pm \sqrt{c_3^2 - 4c_5}}{2}, \\ y &= c_3 - w, \\ z &= \frac{yc_1 - c_4}{y - w}, \\ \zeta &= c_1 - z, \\ v &= \zeta z - c_2 \end{aligned} \tag{32}$$

when $c_3^2 - 4c_5 < 0$ and there is no real solution for (31). That is (28) cannot be converted into the form of (29) in real domain. In order to use the criterion given by (18) or (19), the following two scenarios are considered, respectively.

(i) Consider $c_3^2 - 4c_5 \geq 0$. Equation (28) can be converted into the form of (29) in real domain. Equation (29) can be rewritten as follows in order to use the condition given by (18) or (19):

$$(s + \zeta + w \cdot D)(s + z + y \cdot D) = v, \tag{33}$$

$$\Rightarrow \frac{s + \zeta + wD}{v} = \frac{1}{s + z + yD} := K, \tag{34}$$

$$\Rightarrow \begin{cases} s + \zeta + wD = Kv \\ s + z + yD = \frac{1}{K}, \end{cases} \tag{35}$$

where $K \in C$ is a temporary variable.

Via the first formula in (35), the following equation holds:

$$D = e^{-\tau s} = -\frac{1}{w} (s + \zeta - Kv). \tag{36}$$

According to (15) and (16), with $a_{0,1} = -1/w$, $r_1 = Kv - \zeta$, $c_1 = \tau$, s has the following form:

$$s = S_1(s) = r_1 + \frac{W(z_1)}{c_1}, \tag{37}$$

where

$$z_1 = f_1(\tau) = \frac{c_1 e^{-c_1 r_1}}{a_{0,1}}. \tag{38}$$

Via the second formula in (35), the following equation holds:

$$D = e^{-\tau s} = -\frac{1}{y} \left(s + z - \frac{1}{K} \right). \tag{39}$$

Similarly, having defined $a_{0,2} = -1/y$, $r_2 = 1/K - z$, $c_2 = \tau$, the following result can be obtained:

$$s = S_2(s) = r_2 + \frac{W(z_2)}{c_2}, \tag{40}$$

where

$$z_2 = f_2(\tau) = \frac{c_2 e^{-c_2 r_2}}{a_{0,2}}. \tag{41}$$

Equations (37) and (40) can be utilized to solve the values of s and K when τ is given. They can be further taken into (38) and (41) to get the values of z_1 and z_2 . And if any one of the following equations holds, there is an OEB bifurcation:

$$z_1 = -\frac{1}{e}, \tag{42}$$

$$\frac{d \operatorname{Re}(z_1)}{d\tau} = \frac{d \operatorname{Re}(f_1)}{d\tau} < 0,$$

$$z_2 = -\frac{1}{e}, \tag{43}$$

$$\frac{d \operatorname{Re}(z_2)}{d\tau} = \frac{d \operatorname{Re}(f_2)}{d\tau} < 0.$$

Obviously, if s is a complex eigenvalue, K defined by (34) and z_1, z_2 given by (38) and (41) are all complex values. They are all real values if s is a real eigenvalue. Hence, condition (19) is suitable for this case.

(ii) Consider $c_3^2 - 4c_5 < 0$. Since (28) cannot be converted into the form of (29) in real domain at this condition, it is needed to find a new method for converting (28) into the following form:

$$(s + \zeta + w \cdot D)(s + z + y \cdot D) - q \cdot D \cdot s - v = 0, \tag{44}$$

where $\zeta, y, w, v, z, q \in R$. Also, its expansion is given as follows:

$$\begin{aligned} s^2 + (\zeta + z)s + (\zeta z - v) \\ + (w + y - q)Ds + (wz + \zeta y)D + wyD^2 = 0. \end{aligned} \tag{45}$$

Comparing it with (28), the following equations hold:

$$\begin{aligned} \zeta + z &= c_1, \\ \zeta z - v &= c_2, \\ w + y &= c_3 + q, \\ wz + \zeta y &= c_4, \\ wy &= c_5. \end{aligned} \tag{46}$$

Hence,

$$w = \frac{c_3 + q \pm \sqrt{(c_3 + q)^2 - 4c_5}}{2}, \quad (47)$$

$$y = c_3 + q - w = \frac{c_3 + q \mp \sqrt{(c_3 + q)^2 - 4c_5}}{2}, \quad (48)$$

$$z = \frac{yc_1 - c_4}{y - w}, \quad (49)$$

$$\zeta = c_1 - z, \quad (50)$$

$$v = \zeta z - c_2. \quad (51)$$

To guarantee that ζ, y, w, v, z are real numbers, the following relationship must hold:

$$(c_3 + q)^2 - 4c_5 \geq 0. \quad (52)$$

Since q can be selected arbitrarily, it is set as follows:

$$q = -c_3 + \sqrt{5c_5}. \quad (53)$$

Substituting (53) into (51) yields

$$w = \frac{c_3 + q \pm \sqrt{(c_3 + q)^2 - 4c_5}}{2} = \frac{(\sqrt{5} \pm 1)\sqrt{c_5}}{2}, \quad (54)$$

$$y = c_3 + q - w = \frac{(\sqrt{5} \mp 1)\sqrt{c_5}}{2}.$$

Since $c_3^2 - 4c_5 < 0$, it must be true that $c_5 > 0$. So w and y are two real numbers. According to (49)–(51), ζ, v, z are all real numbers. In order to use condition (19), (44) is written as

$$(s + \zeta + wD)(s + z + yD) = v + qDs, \quad (55)$$

$$\Rightarrow \frac{s + \zeta + wD}{qDs + v} = \frac{1}{s + z + yD} := K, \quad (56)$$

$$\Rightarrow \begin{cases} s + \zeta + wD = K(v + qDs) \\ s + z + yD = \frac{1}{K}. \end{cases} \quad (57)$$

It can be indicated that the second formula in (57) is equivalent to the one in (35). Thus, it can generate the same results given by (40), (41), and condition (43). The new conditions will be derived from the first formula in (57) as follows:

$$s + \zeta + wD = K(v + qDs) \quad (58)$$

$$\Rightarrow D(Kqs - w) = s + \zeta - Kv$$

$$\Rightarrow D = e^{-\tau s} = \frac{s + \zeta - Kv}{Kqs - w} := \frac{P_n(s)}{P_d(s)}. \quad (59)$$

Suppose that there exists a real variable $Q \in \mathbb{R}$ such that

$$e^{-Q\tau s} = \text{sign}(P_n(s)) \cdot (s + \zeta - Kv). \quad (60)$$

Inserting it into (59) yields

$$e^{-(1-Q)\tau s} = \frac{\text{sign}(P_d(s))}{Kqs - w}. \quad (61)$$

Defining $a_{0,3} = \text{sign}(P_n(s)), r_3 = Kv - \zeta, c_3 = Q\tau$, eigenvalue s is expressed as

$$s = S_3(s) = r_3 + \frac{W(z_3)}{c_3}, \quad (62)$$

where

$$z_3 = f_3(\tau) = \frac{c_3 e^{-c_3 r_3}}{a_{0,3}}. \quad (63)$$

Defining $a_{0,4} = \text{sign}(P_d(s)) \cdot Kq, r_4 = w/Kq, c_4 = (Q-1)\tau$, the similar result from (61) is obtained:

$$s = S_4(s) = r_4 + \frac{W(z_4)}{c_4}, \quad (64)$$

where

$$z_4 = f_4(\tau) = \frac{c_4 e^{-c_4 r_4}}{a_{0,4}}. \quad (65)$$

Equations (40), (62), and (64) can be used to solve the values of s, K , and Q when τ is given. They can be further taken into (41), (63), and (65) to get the values of z_2, z_3 , and z_4 . As a conclusion, any of the following conditions hold, and there is an OEB bifurcation in the system:

$$z_2 = -\frac{1}{e},$$

$$\frac{d \text{Re}(z_2)}{d\tau} = \frac{d \text{Re}(f_2)}{d\tau} < 0,$$

$$z_3 = -\frac{1}{e},$$

$$\frac{d \text{Re}(z_3)}{d\tau} = \frac{d \text{Re}(f_3)}{d\tau} < 0,$$

$$z_4 = -\frac{1}{e},$$

$$\frac{d \text{Re}(z_4)}{d\tau} = \frac{d \text{Re}(f_4)}{d\tau} < 0. \quad (66)$$

4.3. High-Dimensional Systems. Consider system Σ given by (1) with $n \geq 3$. Its characteristic equation has the following general form:

$$\text{CE}(s, D) = \sum_{i=0}^n [p_{n-i}(s) D^i] = 0, \quad (67)$$

where $D = e^{-\tau s}$ and $p_{n-i}(s)$ is a polynomial of s :

$$p_{n-i}(s) = \sum_{j=0}^{n-i} a_j s^j. \quad (68)$$

TABLE 1: General forms of the characteristic equation for time-delayed system.

Dim	General forms of the characteristic equation	N_c
1	$s + a_1 + a_2 D = 0$	2
2	$s^2 + a_1 s + a_2 + (a_3 s + a_4) D + a_5 D^2 = 0$	5
3	$s^3 + a_1 s^2 + a_2 s + a_3 + (a_4 s^2 + a_5 s + a_6) D + (a_7 s + a_8) D^2 + a_9 D^3 = 0$	9
4	$s^4 + a_1 s^3 + a_2 s^2 + a_3 s + a_4 + (a_5 s^3 + a_6 s^2 + a_7 s + a_8) D + (a_9 s^2 + a_{10} s + a_{11}) D^2 + (a_{12} s + a_{13}) D^3 + a_{14} D^4 = 0$	14
5	$s^5 + a_1 s^4 + a_2 s^3 + a_3 s^2 + a_4 s + a_5 + (a_6 s^4 + a_7 s^3 + a_8 s^2 + a_9 s + a_{10}) D + (a_{11} s^3 + a_{12} s^2 + a_{13} s + a_{14}) D^2 + (a_{15} s^2 + c_{16} s + a_{17}) D^3 + (a_{18} s + a_{19}) D^4 + a_{20} D^5 = 0$	20

Some general forms of the characteristic equation for system Σ are listed in Table 1. N_c is the number of coefficients in the general form. For example, there are five coefficients which are $a_1 \sim a_5$ in the characteristic equation for $n = 2$, and there are nine coefficients $a_1 \sim a_9$ in the characteristic equation with $n = 3$.

(i) *3-Dim Case ($n = 3$)*. Take 3-dim system as an example to explain the principle of proposed method. General form of the characteristic equation for $n = 3$ is given as below:

$$CE_3(s, D) = s^3 + a_1 s^2 + a_2 s + a_3 + (a_4 s^2 + a_5 s + a_6) D + (a_7 s + a_8) D^2 + a_9 D^3 = 0. \tag{69}$$

It can be converted into the following form so as to utilize the previous results:

$$CE_3(s, D) = CE_2(s, D) \cdot (s + c_6 + c_7 D) - (c_8 s + c_9) = 0, \tag{70}$$

where $CE_2(s, D)$ is described by (28). And, $c_i \in R, i = 1, 2, \dots, 9$, are variables to be determined. Setting $CE_2(s, D) = K$, (70) can be written as

$$\begin{aligned} CE_2(s, D) - K &= 0, \\ K \cdot (s + c_6 + c_7 D) - (c_8 s + c_9) &= 0. \end{aligned} \tag{71}$$

Via the first formula in (71),

$$CE_2'(s, D) := CE_2(s, D) - K = s^2 + c_1 s + (c_2 - K) + c_3 D s + c_4 D + c_5 D^2 = 0. \tag{72}$$

It is obvious that $CE_2'(s, D)$ is a typical 2-dim case discussed above. Hence, the result of Section 4.2 can be directly applied to (72).

Further, via the second formula of (71),

$$K \cdot (s + c_6 + c_7 D) - (c_8 s + c_9) = 0 \implies s - \tilde{a} - \tilde{b} \cdot D = 0, \tag{73}$$

where $\tilde{a} = (c_9 - Kc_6)/(K - c_8), \tilde{b} = -Kc_7/(K - c_8)$. The result of 1-dim system in Section 4.1 can be applied to (73). And the following result can also be derived:

$$z_5 = f_5(\tau) = \tilde{b} \cdot \tau \cdot e^{-\tau \tilde{a}}. \tag{74}$$

From the above discussion, it can be asserted that a 3-dim system can be transformed to a combination of a 1-dim system and a 2-dim system. Therefore, conclusions in Sections 4.1 and 4.2 can be applied. For simplification, it is denoted as

$$CE_3(s, D) = CE_2(s, D) \oplus CE_1(s, D). \tag{75}$$

As a conclusion, any of the following conditions hold, and there is an OEB bifurcation in the system:

$$z_1 = -\frac{1}{e}, \tag{76}$$

$$\frac{d \operatorname{Re}(z_1)}{d\tau} = \frac{d \operatorname{Re}(f_1)}{d\tau} < 0,$$

$$z_2 = -\frac{1}{e}, \tag{77}$$

$$\frac{d \operatorname{Re}(z_2)}{d\tau} = \frac{d \operatorname{Re}(f_2)}{d\tau} < 0,$$

$$z_5 = -\frac{1}{e}, \tag{78}$$

$$\frac{d \operatorname{Re}(z_5)}{d\tau} = \frac{d \operatorname{Re}(f_5)}{d\tau} < 0,$$

where (76) and (77) are concluded from (72) with conditions expressed by (42)-(43) when $c_3^2 - 4c_5 \geq 0$ (or conditions expressed by (66) when $c_3^2 - 4c_5 < 0$).

(ii) *Case of High Dimension with $n > 3$* . Similar to 3-dim case, the characteristic equation of high-dimensional system can also be converted into lower ones so as to apply the previous derived results. For example, for $n = 4$,

$$CE_4(s, D) = CE_3(s, D) \cdot (s + c_{10} + c_{11} D) - (c_{12} s^2 + c_{13} s + c_{14}) = 0. \tag{79}$$

Setting $CE_3(s, D) = K$, (79) can be rewritten as

$$CE_3(s, D) - K = 0,$$

$$CE_4(s, D) \tag{80}$$

$$= K \cdot (s + c_{10} + c_{11} D) - (c_{12} s^2 + c_{13} s + c_{14}) = 0.$$

TABLE 2: z_1, z_2 values near point Q in Figure 10.

τ	$\text{Re}(z_1)$	$\text{Re}(z_1) + 1/e$	$\text{Re}(z_2)$	$\text{Re}(z_2) + 1/e$
0.04758	-0.3675333	0.0003462	-0.0858096	0.2820698
0.04759	-0.3676635	0.0002159	-0.0865306	0.2813488
0.04760	-0.3678304	0.0000491	-0.0879570	0.2799224
0.04761	-0.3679437	-0.0000643	-0.0883511	0.2795284
0.04762	-0.3680362	-0.0001567	-0.0883415	0.2795379

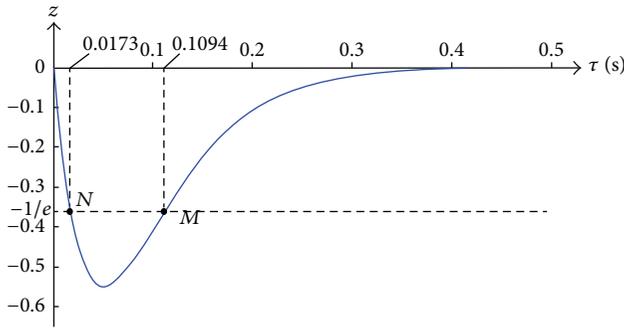
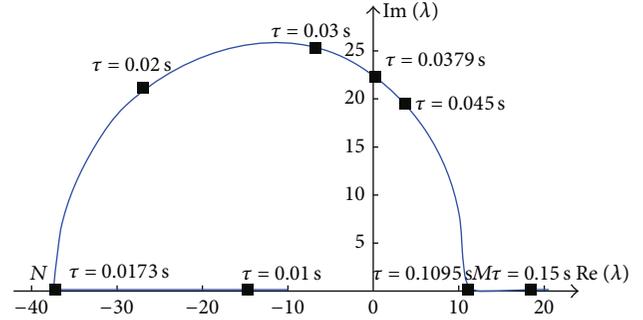
FIGURE 6: Curve of τ - z .

FIGURE 7: Curve of an eigenvalue.

The first formula is a 3-dim case, and the second is a 2-dim case. Hence,

$$\begin{aligned} \text{CE}_4(s, D) &= \text{CE}_3(s, D) \oplus \text{CE}_2(s, D) \\ &= [\text{CE}_2(s, D) \oplus \text{CE}_1(s, D)] \oplus \text{CE}_2(s, D). \end{aligned} \quad (81)$$

And, the cases discussed for 2-dim and 1-dim cases can be applied to determine OEB bifurcation in 4-dim system.

Further, the following recursion formula for high-dimensional systems with $n \geq 3$ can be obtained:

$$\text{CE}_i(s, D) = \text{CE}_{i-1}(s, D) \oplus \text{CE}_{i-2}(s, D), \quad i = 3, 4, \dots \quad (82)$$

Then, a higher dimension system can be converted into two lower dimension systems so as to determine the occurrence of OEB bifurcation accordingly.

5. Case Studies

5.1. 1-Dim System. Consider the following 1-dim system:

$$\dot{x} = 20x - 30x(t - \tau). \quad (83)$$

According to (24), the τ - z curve can be depicted in Figure 6 and the corresponding eigenvalue locus is depicted in Figure 7. For a pair of conjugated eigenvalues, only the one above the real axis is showed in the figures in this paper.

Similar to Figure 5, point N with $(\tau, z) = (0.0173s, -1/e)$ in Figure 6 is an OEB bifurcation of system described by (83). The variation of the system eigenvalue in Figure 7 verifies the analysis above. That is, the real eigenvalue splits into a pair of conjugated complex eigenvalues at the OEB bifurcation with $\tau = 0.0173s$.

In order to demonstrate the impact of OEB bifurcation to the system defined by (83), its unit step responses with

different τ values are shown in Figure 8. It can be found that the system trajectory converges monotonously in the range of $\tau < 0.0173s$ and converges oscillatedly in the range of $\tau > 0.0173s$. It is manifested that there is OEB bifurcation at $\tau = 0.0173s$, which leads to a new oscillation mode and increases the number of system eigenvalues by one.

5.2. 2-Dim System. The following two cases are employed to validate the proposed method.

(i) Case A. Consider

$$\begin{aligned} \mathbf{A}_0 &= \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} = \begin{bmatrix} 1 & -3 \\ 5 & -6 \end{bmatrix}, \\ \mathbf{A}_i &= \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix} = \begin{bmatrix} -4 & 4 \\ 2 & -3 \end{bmatrix}, \end{aligned} \quad (84)$$

$$\text{eig}(\bar{\mathbf{A}}) = [-2.0, -10.0],$$

$$c_3^2 - 4c_5 = 33.0 > 0,$$

where $\bar{\mathbf{A}}$ is defined by (26).

It is obvious that the conditions described by (42)-(43) are suitable for this case.

Via the tracing method proposed by [23], we can obtain the system eigenvalue locus. Figure 9 depicts the curve of the second eigenvalue with τ increasing (the first one is always on the real axis, so it is not shown in the figure). There is an OEB bifurcation at point Q with $\tau = 0.0476s$. According to (38) and (41), the curves of τ - z_1 and τ - z_2 can be depicted in Figure 10. Solid line represents that the corresponding z_i , $i = 1, 2$, is real, while dotted line represents that it is complex. Some results nearby point Q are listed in Table 2. It can be found that condition (42) holds at point Q with

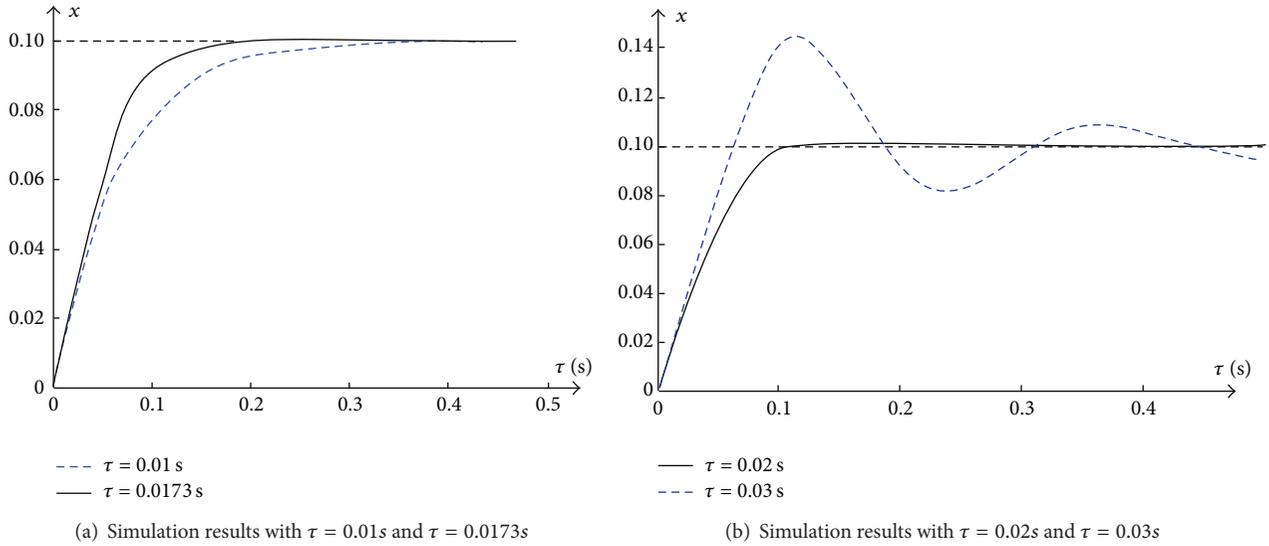


FIGURE 8: Simulation results with various τ values.

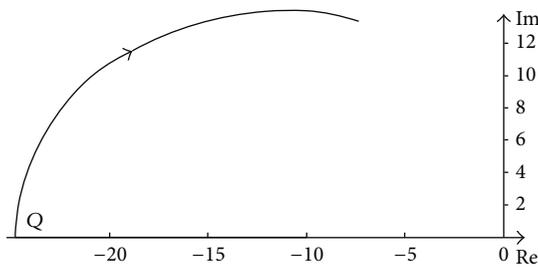


FIGURE 9: Locus of the second eigenvalue with τ increasing.

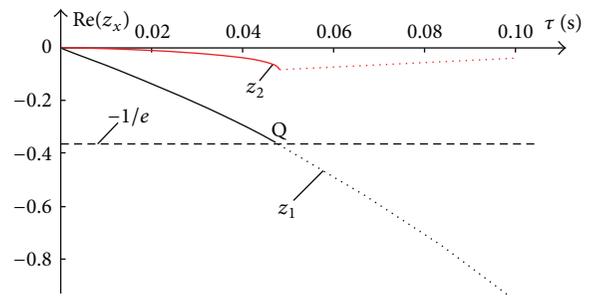


FIGURE 10: Curves of $\tau - z_1$ and $\tau - z_2$.

$(\tau, z_1)_R = (0.0476\text{s}, -1/e)$ and it indicates the occurrence of OEB bifurcation precisely.

(ii) Case B. Consider

$$\begin{aligned}
 \mathbf{A}_0 &= \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} = \begin{bmatrix} 1 & 2 \\ 5 & -6 \end{bmatrix}, \\
 \mathbf{A}_i &= \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix} = \begin{bmatrix} -4 & -1 \\ 2 & -3 \end{bmatrix}, \\
 \text{eig}(\bar{\mathbf{A}}) &= [-2.0, -10.0], \\
 c_3^2 - 4c_5 &= -7.0 < 0,
 \end{aligned} \tag{85}$$

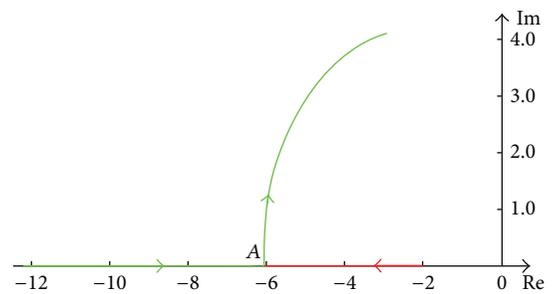


FIGURE 11: Eigenvalue locus of Case B.

where $\bar{\mathbf{A}}$ is defined by (26).

It can be asserted that the conditions described by (66) are appropriate for this case. Similar to Case A, the eigenvalue locus with τ increasing can be obtained via the tracing method expressed by [23]. The eigenvalue locus is shown in Figure 11, while real and imaginary parts of the eigenvalues are shown in Figure 12. Note that two real eigenvalues at the beginning move close to each other on the real axis. They encounter at point A and then turn to a pair of conjugated complex eigenvalues. According to Definition 1,

there is no OEB bifurcation in the system since the number of eigenvalues does not increase here.

Figure 13 plots the curves of $\tau - z_2$, $\tau - z_3$, and $\tau - z_4$. Similarly, solid and dotted lines are used to represent the real and complex values of z_i , $i = 2, 3, 4$. It is obvious that any condition identified by (66) does not hold here, so there is no OEB bifurcation in the system.

Case studies above demonstrate that conditions expressed by (42)-(43) or (66) are correct. And, the method proposed

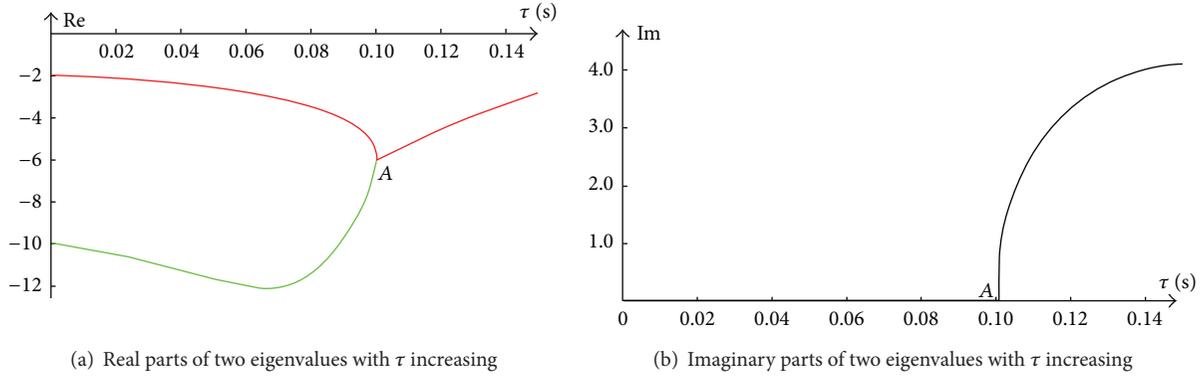


FIGURE 12: Real and imaginary parts of two eigenvalues.

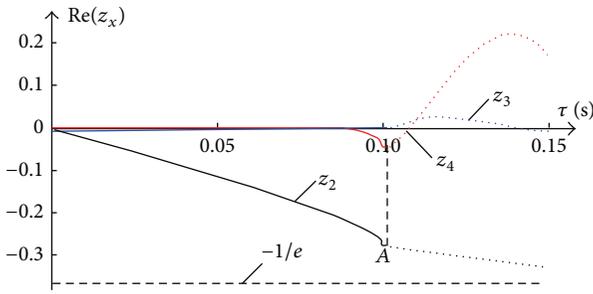


FIGURE 13: Curves of $\tau-z_2$, $\tau-z_3$, and $\tau-z_4$.

can correctly indicate the occurrence of OEB bifurcation in the 2-dim time-delayed system.

5.3. 3-Dim System. Consider a 3-dim system defined by (1) with A_0, A_i as follows:

$$A_0 = \begin{bmatrix} -5 & 1 & -1 \\ 1 & -4 & 2 \\ 0 & 0 & -2 \end{bmatrix}, \quad A_i = \begin{bmatrix} 2 & 1 & 0 \\ 1 & -1 & -1 \\ 1 & 3 & -8 \end{bmatrix}. \quad (86)$$

It can be found that the system have three real eigenvalues with $\tau = 0$:

$$\text{eig}(\bar{A}) = [-1.8692, -5.5749, -10.5559], \quad (87)$$

where $\bar{A} = A_0 + A_i$.

Similar to Section 5.2, we can get the eigenvalue locus shown in Figure 14, where the first and second eigenvalues always move on the real axis, while the third eigenvalue splits into a pair of conjugated complex eigenvalues at point B with $\tau = 0.0431s$ so as to yield an OEB bifurcation.

Table 3 gives the coefficients in (69) and (70). According to the definition of z_1, z_2, z_5 by (76)–(78), we can depict the curves of $\tau-z_1, \tau-z_2$, and $\tau-z_5$ in Figure 15. The $\tau-z_5$ curve (red line) hits the horizontal line of $-1/e$ at $\tau = 0.0431s$ and condition (78) holds which indicate the occurrence of the OEB bifurcation.

It should be mentioned that the transformation from (69) to (70) is not unique. Table 4 shows two sets of coefficients

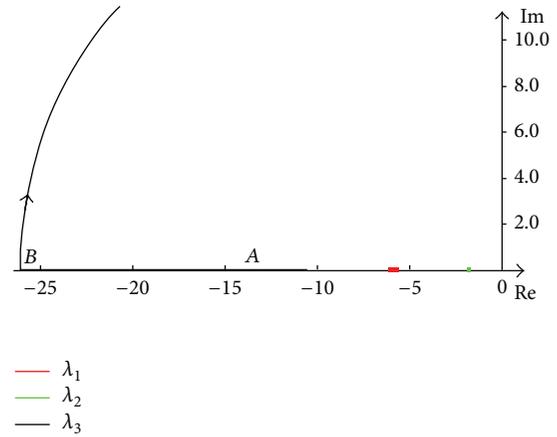


FIGURE 14: Eigenvalue locus with time delay increasing.

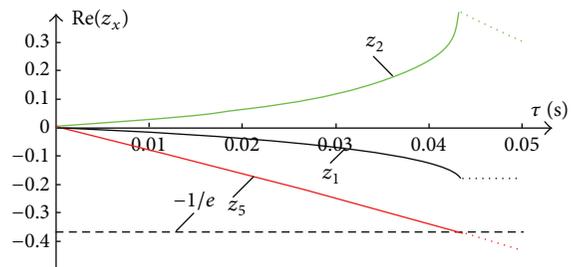


FIGURE 15: Curves of $\tau-z_1$, $\tau-z_2$, and $\tau-z_5$.

in (70). The corresponding $\tau-z_1, \tau-z_2$, and $\tau-z_5$ curves are illustrated, respectively, by Figures 16 and 17. It is notable that in Figure 16 or Figure 17, the $\tau-z_1$ curve (black line) collides with the horizontal line of $-1/e$ at $\tau = 0.0431s$. The condition of (76) holds at this point so as to indicate occurrence of the OEB bifurcation.

From the case study above, it is verified that conditions expressed by (76)–(78) can indicate the occurrence of OEB bifurcation in the 3-dim time-delayed LTI system.

TABLE 3: Coefficients of $CE_3(s, D)$ given by (69) and (70).

a_1	a_2	a_3	a_4	a_5	a_6	a_7	a_8	a_9
11	37	38	7	60	117	-8	-16	-29
c_1	c_2	c_3	c_4	c_5	c_6	c_7	c_8	c_9
8.2422	15.7565	-0.5508	-0.7162	-3.8406	2.7578	7.5508	1.4870	5.4538

TABLE 4: Two sets of coefficients in (70).

	c_1	c_2	c_3	c_4	c_5	c_6	c_7	c_8	c_9
Set I	6.4863	13.8753	9.2544	32.8516	12.8635	4.5137	-2.2544	6.1525	24.6287
Set II	7.2715	7.6935	5.2964	27.8647	-17.0229	3.7285	1.7036	-2.1947	-9.3149

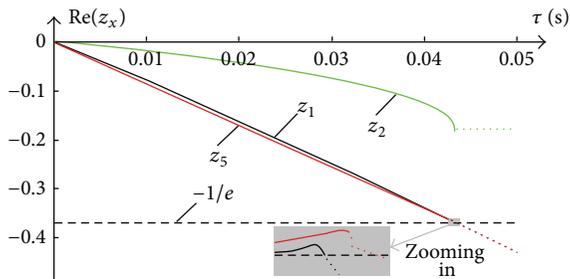


FIGURE 16: Curves of $\tau-z_1$, $\tau-z_2$, and $\tau-z_5$ with set I of Table 4.

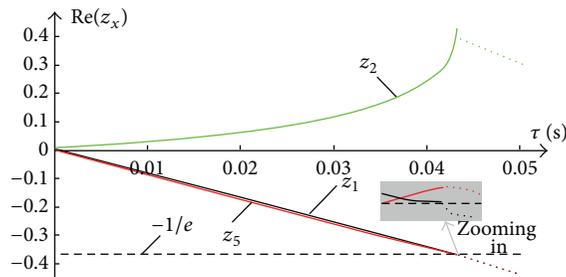


FIGURE 17: Curves of $\tau-z_1$, $\tau-z_2$, and $\tau-z_5$ with set II of Table 4.

6. Conclusions

In this paper, a method based on Lambert W function theory is presented to determine the oscillation emergence bifurcation (OEB) in time-delayed LTI system with single lag. Conditions of OEB's occurrence in 1-dim, 2-dim, 3-dim, and higher dimension systems are derived, respectively. And, case studies confirm the correctness and preciseness of the proposed method. Work of this paper is beneficial to explore the complex dynamic phenomena existing in the time-delayed system. However, the proposed method is only valid for the time-delayed system with single lag. How to expand it to the multiple time-delayed dynamic systems will be further discussed in the future.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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