

$L(S) = L(S_1) + L(S_2)$ (Rado and Reichelderfer, *On a stretching process for surfaces*, Amer. J. Math. vol. 61 (1939)). (Received November 28, 1942.)

57. Antoni Zygmund: *A property of the zeros of Legendre polynomials.*

Suppose that $n < m$ are positive integers and that a polynomial $\phi(x)$ of degree n does not exceed M in absolute value at the zeros of the Legendre polynomial $P_m(x)$. Then $|\phi(x)| \leq A(\delta)M$ for $-1 \leq x \leq +1$, where $A(\delta)$ depends only on the number δ defined by the equations $m/n = 1 + \delta$. Similar results hold for the integrals $\int_{-1}^{+1} |\phi(x)|^r dx$ with $r \geq 1$. (Received November 23, 1942.)

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58. Stefan Bergman: *A formula for the stream function of compressible fluid flow.*

Let $q = ve^{i\theta}$ denote the velocity vector. A flow, \mathcal{F} is said to be of the type D_n , if the boundary of the domain, B , in which \mathcal{F} is defined consists of $2n$ segments S_K such that along each S_{2K} , $K = 1, 2, \dots, n$, $\theta = \theta_K$ is constant and along each S_{2K-1} , v is constant. (S_{2K} are segments of straight lines, S_{2K-1} are so-called "free boundaries.") The image of B in the logarithmic plane (see *Notes on hodograph method in the theory of compressible fluid*, publication of Brown University, p. 6) is a polygonal domain. In the case of an incompressible fluid the stream function of \mathcal{F} can be represented as a closed expression with n parameters. The author considers subsonic flows, \mathcal{C} , of compressible fluid. Using certain linear operators (see above mentioned *Notes*, §§6 and 10, and Trans. Amer. Math. Soc. vol. 53 (1943) pp. 130-155) he derives a similar explicit formula for the flows \mathcal{C} of "nearly type D_n ," that is to say, for flows whose boundaries consist of $2n$ segments along which θ or v assume nearly constant values. The angles θ_K may be prescribed. (Received November 21, 1942.)

59. R. M. Foster: *On the average resistance of an electrical network.*

In an electrical network composed of two-terminal resistance elements, let J designate the total resistance measured across the terminals of an element, the internal resistance of this element being r_i , and let S_i be the driving-point resistance measured in the branch containing this element r_i . It is shown in this paper that, for any network configuration whatsoever, $\sum J_i/r_i = R$ and $\sum r_i S_i = N$ (the summation being extended over all the elements of the network), with $R = V - P$ and $N = E - V + P$, where E is the number of elements, V the number of vertices, and P the number of separate, unconnected parts of the configuration. The average values of the ratios J_i/r_i and r_i/S_i are thus R/E and N/E , respectively. If all the elements of the network have the same internal resistance r , and if there is complete symmetry among the elements so that the resistance measured across any one element is necessarily equal to that across any other element, then $J_i = rR/E$ and $S_i = rE/N$. These results are extended to generalized impedances, and to infinite networks. (Received November 23, 1942.)

60. A. H. Fox: *Integral representation of the flow of a compressible fluid around a cylinder.*

The steady irrotational two-dimensional flow of a compressible fluid may be approximated by the flow of a hypothetical incompressible fluid in which the pressure is